

♦ DESCRIPTION

The MT1523 is a high efficiency DC/DC buck regulator with a built-in power MOSFET. It can conduct 2A continuous output current over a wide input supply range from 4.75V to 18V with excellent load and line regulation.

The output is adjustable down to 0.92V. The MT1523 operates in current mode which provides fast transient response, easy compensation and cycle-by-cycle current limiting.

The MT1523 will shutdown when the temperature is over 160° C. It folds the PWM frequency down to 75KHz when the output is shorted. In shutdown mode the regulator draws $20\mu\text{A}$ of supply current. The MT1523 comes with SOP-8 package and is rated over -40° C and 85° C ambient temperature range.

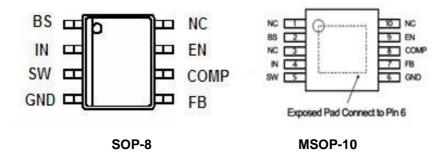
♦ FEATURES

- > High Efficiency: Up to 93%
- 2A Output Current
- ➤ 4.75V to 18V Input Voltage Range
- Fixed 390KHz Frequency
- > 0.2Ω Internal Power MOSFET Switch
- > 20uA Quiescent Current at Shutdown Mode
- Thermal Shutdown
- Cycle-by-Cycle Over-current Protection
- Output Adjustable from 0.92V to 12V
- > Stable with Low ESR Output Ceramic Capacitors
- Available in SOP-8 and MSOP-10 Package with Exposed Pad

♦ APPLICATIONS

- Portable Devices
- LCD Monitors
- Automobile Application
- Battery Charger
- Distributed Power Systems

♦ PIN CONFIGURATIONS





♦ PIN CONFIGURATION

Pin Number	Name	Function			
1 BS		Bootstrap.			
		Connect a 10nF or greater ceramic capacitor from BS to SW. The capacitor			
		supplies the gate drive for the upper side switch of the regulator.			
		Power Supply.			
		IN provides the power to the IC, as well as the step-down switcher. Drive IN with			
2	IN	a voltage source between 4.75V and 18V. Bypass IN to GND with a			
		suitable capacitor to eliminate the noise on the input to the IC.			
		See Input Capacitor.			
	sw	Power Switch Pin.			
3		SW is the switching node that supplies power to the output. Connect the output			
3		LC filter from SW to the output load. Note that a capacitor is required from SW to			
		BS to power the upper side switch.			
4	GND	Ground.			
	FB	Feedback Input.			
_		FB senses through a resistive voltage divider from the output voltage. The			
5		feedback threshold is 0.92V.			
		See Setting the Output Voltage.			
		Compensation Node.			
	СОМР	COMP is used to compensate the regulation control loop. Connect a series RC			
6		network from COMP to GND to compensate the regulation control loop.			
		See Compensation.			
	EN	Enable Input.			
_		EN is a digital input that turns the regulator on or off. Drive EN high to turn on			
7		the regulator; drive EN low to turn it off. For automatic startup, leave EN			
		unconnected.			
8	NC	No Connect.			



♦ ABSOLUTE MAXIMUM RATINGS

Symbol	Parameter	Maximum	Unit
Input Voltage	V_{IN}	-0.3 to 30	V
SW Pin Voltage	V _{SW}	-1 to V _{IN} +1V	V
Bootstrap Voltage	V_{BS}	V_{SW} -0.3 to V_{SW} +6	V
All Other I/O Pin		-0.3 to 6	V
Operating Ambient Temperature	T _A	-20 to 85	°C
Maximum Junction Temperature	TJ	150	°C
Storage Temperature	T _{STG}	-65 to 150	°C
Lead Temperature(Soldering, 10 sec)	T _{LEAD}	260	°C

To prevent permanent damage to the device, do not stress the device beyond these absolute maximum ratings.

♦ RECOMMENDED OPERATING CONDITIONS

Symbol	Parameter	Maximum	Unit	
Input Voltage	V_{IN}	4.75 to 18	V	

♦ POWER DISSIPATION TABLE

	Package θ _{JA} (°C /W) M 90		T _A ≤ 25 °C Power rating(mW)	T _A =70°C Power rating(mW)	T _A = 85 °C Power rating (mW)		
			1389	889	722		
	U	105	1190	762	619		

Note:

 $T_J = T_A + (P_D \times \theta_{JA})$

The θ_{JA} numbers are guidelines for the thermal performance of the device/PC-board system. All of the above assume no ambient airflow.

3. $\theta_{JA:}$ Thermal Resistance-Junction to Ambient.

ORDERING INFORMATION

Device	Package		V _{OUT} Volts	T _A (°C)
MT1523-ADJM	M	SOP-8	ADJ	-20 to 85
MT1523-ADJU	U	MSOP-10	ADJ	-20 to 85

^{1.} Exceeding the maximum allowable power dissipation will result in excessive die temperature, and the regulator will go into thermal shutdown.

^{2.} TJ: Junction Temperature Calculation:



♦ FUNCTIONAL BLOCK DIAGRAM

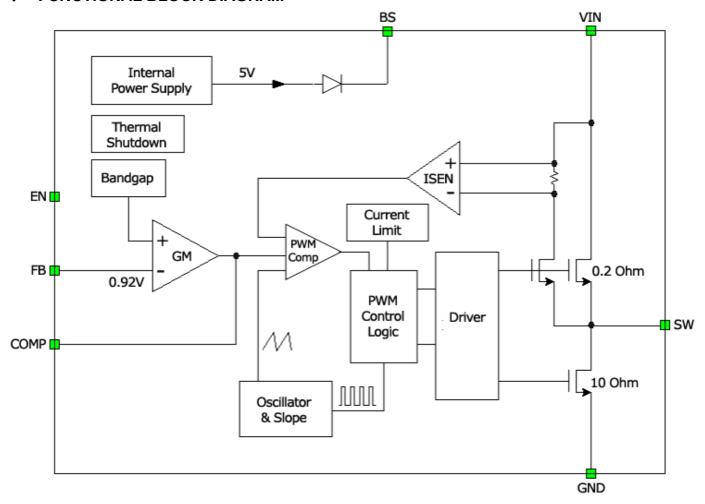


Figure 2. Functional Block Diagram

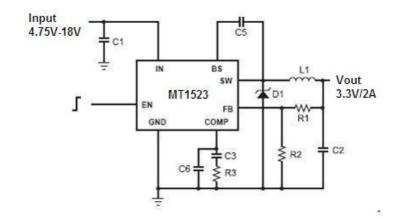


♦ FUNCTIONAL DESCRIPTION

The MT1523 is a high efficiency DC/DC buck converter. It regulates input voltages from 4.75V to 18V down to a programmable output voltage as low as 0.92V, and is able to supply up to 2A of continuous load current. The MT1523 uses current-mode PWM control at a fixed frequency of 390KHz. The output voltage is sensed at FB pin through a resistive voltage divider and fed into the internal transconductance error amplifier. The difference of FB and the internal reference (0.92V) is then integrated to get the COMP voltage through an R-C network which also compensates the regulation control system. The COMP voltage is then compared to the signal representing the sensed switch current to get the right PWM.

The converter uses an internal n-channel MOSFET switch to step down the input voltage to the regulated output voltage. Since a gate voltage greater than the input is required, a bootstrap cap is connected between SW and BS to drive the gate of the upper switch. The capacitor is internally charged to 5V while the upper switch is off. An internal 10 lower switch from SW to GND is used to insure that SW is pulled to GND when charging the bootstrap capacitor. The IC will thermal shutdown when the temperature is over 160 °C. When output is shorted, the oscillator will fold its frequency down to 75KHz to protect the IC.

TYPICAL APPLICATIONS



◆ TEST CIRCUIT

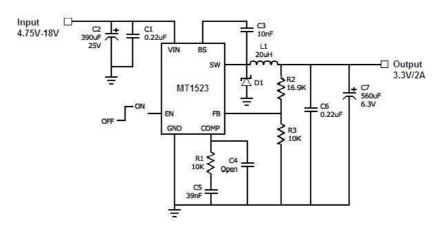


Figure 3. MT1523 Step Down from 18V to 3.3V @2A



♦ ELECTRICAL CHARACTERISTICS

 $(V_{IN} = 12V, V_{EN} = 5V, unless otherwise specified refer to circuit of Figure 3. Typical values are at T_A = 25 oC.)$

Parameter	Symbol	Conditions	Min.	Тур.	Max.	Unit
Feedback Pin Voltage	V _{FB}	4.75V ≤ V _{IN} ≤ 18V	0.893	0.920	0.947	V
Upper Switch On Resistance	Ron_up		-	0.2	-	Ω
Lower Switch On Resistance	Ron_low		-	10	-	Ω
Upper Switch Leakage	ILEAK	V _{EN} = 0V, V _{SW} = 0V	-	_	10	μA
Current Limit	Ішміт		2.4	2.8	-	Α
Oscillator Frequency	Fosc		330	390	450	KHz
Short Circuit Frequency	Fsc	V _{FB} = 0V	-	75	-	KHz
Maximum Duty Cycle	Dмах	V _{FB} = 1V	-	90	-	%
Minimum Duty Cycle	DMin	V _{FB} = 1V	-	_	0	%
Error Amplifier	0			750		
Transconductance	GEA		-	750	-	μA/V
EN Threshold	VTHR		0.8	1.1	1.4	V
Under Voltage Lockout	1 .,		2.0	2.5	3.0	V
Threshold Rising	Vuvlo		2.0			
Under Voltage Lockout	VHYS			200	-	mV
Threshold Hysteresis	VHYS		-			
Shutdown Supply Current	Isp	V _{EN} = 0V	-	20	50	μΑ
Operating Supply Current	ЮР	V _{EN} = 0V, V _{FB} = 1.4V	-	1.0	-	mA
Thermal Shutdown	Tsp		-	160	-	°C

Notes:

- 1. Measured on 1" square of 1 oz. copper FR4 board.
- 2. Exceeding the absolute maximum rating may damage the device.
- 3. The device is not guaranteed to function outside its operating ratings

◆ APPLICATION INFORMATION

Setting the Output Voltage

A resistive voltage divider from the output to GND (see Figure 3) is used to set the output voltage. The voltage divider divides the output voltage down to FB by the ratio:

$$V_{FB} = V_{OUT} * R3/(R2 + R3)$$

VFB is internally set at 0.92V. Thus the output voltage is:

$$V_{OUT} = 0.92*(R2+R3)/R3$$

If we set R3=10 $K\Omega$, R2 is determined by:

$$R2 \cong 8.18 * (V_{OUT} - 0.92)(K\Omega)$$

For example, for a 3.3V output voltage, R2 is 16.9. $K\Omega$

Input Capacitor

An input capacitor C1 is required to filter the noise of the input to the step-down converter. The bypass capacitor should be placed close to the IN pin and GND. A low ESR capacitor is recommended to keep the noise at the IC to a minimum. Ceramic capacitors are preferred, but tantalum or low-ESR electrolytic capacitors may also suffice. The input capacitor is recommended to be greater than 10µF in value with right voltage rating (higher than the input voltage). However since it absorbs the input switching current it requires an adequate ripple current rating. Its RMS current rating should be greater than approximately 1/2 of the DC load current. Alternatively we could place a small high quality ceramic 0.1µF capacitor (C1) closer to the IC and a larger capacitor (C2) farther away. If using this technique, it is recommended that C2 be a tantalum or electrolytic type. All ceramic capacitors should be placed close to the IC.

Output Capacitor

The output capacitor together with the inductor serves as filter to maintain the DC output voltage. Increasing the output capacitance will lower the output ripple and improve load transient response but increase the solution size and cost. The characteristics of the output capacitor also affect the stability of the regulation control system. Low ESR capacitors are preferred to keep the output voltage ripple low. Ceramic, tantalum, or low ESR electrolytic capacitors are recommended. In the case of ceramic capacitors, the output voltage ripple is mostly independent of the ESR and can be estimated to be:

◆ APPLICATION INFORMATION (Continue)

$$V_{\text{RIPPLE}} \cong 1.4 * V_{\text{IN}} * \left(f_{\text{LC}} / f\right)^2$$

Where VRIPPLE is the output ripple voltage, VIN is the input voltage, fLC is the resonant frequency of the LC filter, f is the switching frequency. In the case of tantalum or low-ESR electrolytic capacitors, the ESR dominates the impedance at the switching frequency, and so the output ripple is calculated as:

$$V_{RIPPLE} \cong \Delta I * R_{ESR}$$

Where ΔI is the inductor ripple current, and RESR is the equivalent series resistance of the output capacitors. The alternative method used for input capacitor can also be applied here, with a small high quality ceramic cap close to the IC and a tantalum or electrolytic cap next to it.

Inductor Selection

The selection of the inductor is determined by the following factors: (a) inductance; (b) rated current value; (c) size requirement; (d) DC resistance (DCR). Increasing the value of the inductor can reduce ripple current but increase the physical size, DCR, and/or lower saturation current. To allow the peak-to-peak ripple current in the inductor to be approximately 30% of the maximum load current, we can determine the inductance by:

$$L = V_{OUT} * (V_{IN} - V_{OUT}) / (V_{IN} * f * \Delta I)$$

Also make sure the peak current of inductor is less than the current limit.

$$I_{PEAK} = I_{IOAD} + \Delta I/2$$

Schottky Diode Selection

Schottky diode is used to supply current when the upper switch is off. The following factors should be considered: (a) maximum reverse voltage rating higher than input voltage; (b) current rating higher than load current; (c) forward voltage which affects the efficiency.

Compensation

The system stability is compensated through the COMP pin. A series R-C network connected to COMP provides a pole-zero pair to stabilize the system.

The DC loop gain is:

$$A_{VDC} = (V_{FB} / V_{OUT}) * A_{VEA} * G_{CS} * R_{LOAD}$$



◆ APPLICATION INFORMATION (Continue)

Where:

VFB is the feedback threshold voltage, 0.92V. Vout is the desired output regulation voltage. AVEA is the transconductance error amplifier voltage gain, 400 V/V. Gcs is the current sense gain, (roughly the output current divided by the voltage at COMP), 1.95 A/V. RLOAD is the load resistance (or Vout / lout where lout is the output load current) The dominant pole of the system is due to the compensation capacitor (C5):

$$f_{P1} = G_{EA} / (2\pi * A_{VEA} * C_5)$$

where GEA is the EA transconductance (750µA/V).

The second pole is due to the output:

$$f_{P2} = 1/(2\pi *R_{LOAD} *C7)$$

The zero of importance is introduced to the system by the compensation Cap.(C5) and the compensation resistor (R1):

$$fz_1 = 1/(2\pi *R1*C5)$$

If a large value capacitor (C7) with relatively high ESR is used, the zero due to the capacitance and ESR of the output capacitor can be compensated by a third pole set by R1 and C4. The third pole is then located at:

$$f_{P3} = 1/(2\pi *R1*C4)$$

The system crossover frequency (the frequency where the loop gain drops to 1 or 0dB) is set to approximately 1/10 of the switching frequency. In this case, the switching frequency is 390KHz, therefore use a crossover frequency, fc, of 40KHz. Lower crossover frequencies result in slower response and worse transient load recovery. Higher crossover frequencies can result in instability.

Steps to Choose Compensation Components

Step 1. Choose the compensation resistor to set the desired crossover frequency. Determine R1 by the following equation: $R1 = 2\pi *C7 * Vout * fc /(GeA *Gcs * VFB)$

If the equation gives R1 greater than 10K, set R1=10K_ to prevent output overshoot at startup. This will lead to f_c less than the desired 40KHz, and is given by:

$$fc = R1*Gea*Gcs*Vfb/(2\pi*C7*Vout)$$

Step 2. Choose the compensation capacitor C5 to set the zero to 1/4 of the crossover frequency. This gives:

$$C5 = (0.22 *C7 * VouT)/R1$$

Step 3. If the ESR zero of the output capacitor is less than four times the crossover frequency:

$$8\pi *C7 *Resr * fc \ge 1$$

Or:

$$(7.34*10^{-5}*R1*Resr)/Vout \ge 1$$

If this is the case, add the second compensation capacitor. Determine the value by the equation:

$$C4 = C7 *R ESR(MAX)/R1$$

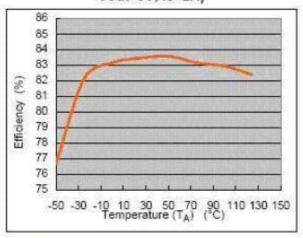
where Resr(MAX) is the maximum ESR of theoutput capacitor.



Efficiency vs. Temperature (Vin=12V,

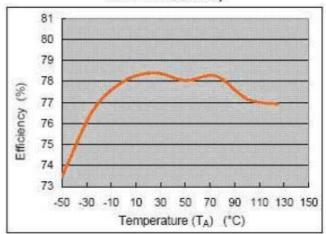
TYPICAL PERFORMANCE CHARACTERISTICS

MT1523 Efficiency vs. Temperature (Vin=12V, Vout=5V, Io=2A)

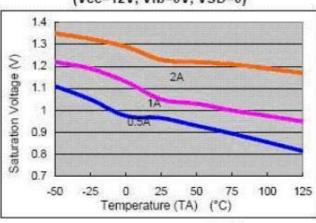


Vout=3.3V, lo=2A)

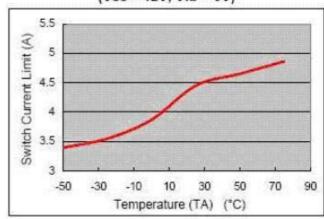
MT1523



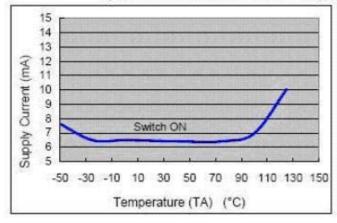
Saturation Voltage vs. Temperature MT1523 (Vcc=12V, Vfb=0V, VSD=0)

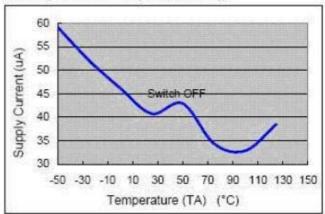


MT1523 Switch Current Limit vs. Temperature (Vcc = 12V, Vfb = 0V)



MT1523 Supply Current vs. Temperature (Vcc=12V, No Load, Von/off =0V(Switch ON), Von/off =5V(Switch OFF))







◆ PHYSICAL DIMENSIONS: SOP-8

